



## EFFECT OF BOTH AMBIENT TEMPERATURE AND SOIL MOISTURE ON THE EARTHING RESISTANCE

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### ABSTRACT

Augmenting the electrical systems reliability can be accomplished by earthing every stage of electricity generation, transmission and utilization. An accurate grounding system resistance calculations recommend to consider the relevant realistic effective parameters. This paper demonstrates the effect of these parameters such as soil types, soil moisture status in terms of the ambient temperature and finally the earthing electrode types and dimensions. This study comprises the common soil moisture statues such as frosty, cool, wetted, liquid, worm or dries for each of boggy, clay, sandy, silty, peaty, chalky, loamy soils. Moisture proportion varies in these soil types that could lead to diversity of soil resistivity. Full description of earthing resistance profile in case of the different soil types, different environmental conditions as well as different electrode types will be presented. Individual MATLAB files for the different electrodes types will be developed. This work extends the soil moisture states and their effects throughout the whole earthing calculations. The system point by point results are in successfully agreements with the corresponding ETAP results.

**Keywords :** Earthing system, electrodes, moisture, touch, step voltages, and fault current.

### INTRODUCTION

Grounding is predominately the connection between an electrical system and general mass of earth, the last being soil volume, rock and so on, dimensions are extensive in contrast with the electricity system. It is significant that, in Europe they tend to utilize the expression "Earthing" while in North America, the expression which is more common being "Grounding". The purpose of earthing in electric power facilities is to ensure effective protection of people and animals from injuries inside and outside the substation, as well as technical protection of expensive equipment in power substations. The human being protections, the building safety and the systems life time are always occupying the highest priority of the earthing systems designers concern [1-3]. The earthing systems, in fact have several different topologies. The classifications of these are broadly based on each of:

- Earthed system (power station, hybrid power station, residential homes or appliances).
- Earthing platforms (electrodes, soil and the environmental parameters).

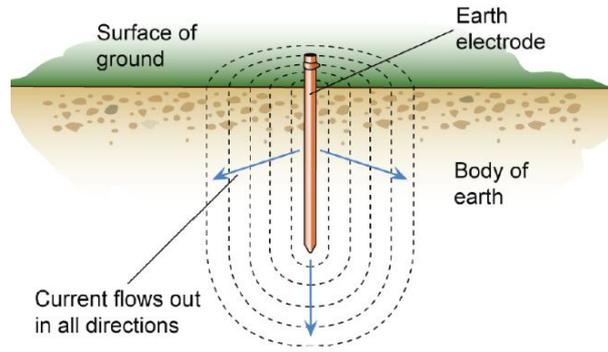
This work high light on the earthing parameters for a wide grounding dynamic range where all earthing electrodes (single rod, multi-rods and grids) can be used. Widest range of the temperature changes, as well as the excepted different soil types are considered.

### Grounding system calculations

However, the high credibility of IEEE std-80 to calculate discretely the grounding resistance for different grounding topologies, the proposed calculations validate a complete resistance description in term of the whole grounding parameters. Summarized analytical calculations of the most dominant ground schemes are listed as follows:

#### Single rod

The single ground rod of fig.1, could offer the cheapest and most convenient means of installing an electrode [4]. The following mathematical formulas [5-16] can be used to calculate the earthing resistance of a single driven rod in uniform soil having resistivity " $\rho$ ".



$$R_{1g} = \frac{\rho}{2\pi L_r} \left[ \ln\left(\frac{8L_r}{d_r}\right) \right] \quad (1)$$

**Fig.1: Single rod [28]**

For more practical consideration the rod is assumed as carrying current uniformly along its length, the earthing resistance can be obtained from:

$$R_{1g} = \frac{\rho}{2\pi L_r} \left[ \ln\left(\frac{8L_r}{d_r}\right) - \frac{1}{2} \right] \quad (2)$$

Where;  $R_g$  is the resistance of the soil in  $\Omega$ ,  $\rho$  is the resistivity of the soil in  $\Omega.m$ ,  $L_r$  is the length of the single rod in m and  $d_r$  is the diameter of the single rod in m.

**Multi-rod**

Although the driven rod is a simple practical method of making an earth connection, its shape does not lend itself to exact calculation. Several approximate formulas for driven rod earthing resistance have been suggested [17]. In the event that the desired soil resistivity is not achievable using a single earth electrode, multiple electrodes could be used. The combined resistance of rod electrodes in parallel can be obtained from the following equations [18]:

$$R_{n_r} = R_1 \left( \frac{1 + \lambda a}{n_r} \right) \quad (3)$$

$$a = \frac{\rho}{2\pi R_1 n_r} \quad (4)$$

Where;  $R_{n_r}$  is the earthing resistance of soil due to using multi-rod,  $S$  is rod spacing in m,  $\rho$  is the soil resistivity in  $\Omega.m$ ,  $R_1$  is the resistance of one footing in  $\Omega$ ,  $\lambda$  is a factor depends on number of rods and  $n_r$  is the number of rods.

**Grid (Lattice)**

Earthing grid of fig.2 in contrast with the single rod and multi-rod systems, allows a higher disperse the fault current into the earth so that the voltage distribution on the surface of the earth will be more uniform. This guarantees an acceptable safety requirement such as reduction of touch and step voltages as well as the grounding resistance. There are in fact, different types of earthing grid design such as square, rectangular, L shaped, T shape, trapezoid, triangular shaped grids [19-23]. Soil resistance can be calculated by using the equation (5) [24].



**Fig.2: Grid earthing scheme [29]**

$$R_{lg} = \left[ \frac{1}{L_T T} + \frac{1}{\sqrt{20A} \left( 1 + \frac{1}{(1 + h\sqrt{20})} \right)} \right] \quad (5)$$

Where,  $L_T$  is total length of grid in m,  $A$  is the area of lattice in  $m^2$  and  $h$  is the depth of lattice in m. The conductor size for substation earth grid is [20]:

$$A_c = I_f \sqrt{\frac{\frac{t_c \cdot \alpha_r \cdot \rho_r \cdot 10^4}{TCAP}}{\ln \left[ 1 + \frac{(T_m - T_a)}{K_0 + T_a} \right]}} \quad (6)$$

Where;  $A_c$  is conductor size in sqr-mm,  $I_f$  is maximum fault current in kA,  $t_c$  is duration of fault in sec,  $\alpha_r$  is thermal coefficient of resistivity at reference temperature,  $\rho_r$  is resistivity of earth electrode at reference temperature  $\mu\Omega/cm$ , TCAP is thermal capacity factor,  $T_m$  is maximum allowable temperature of conductor in  $^\circ C$ ,  $T_a$  is ambient temperature in  $^\circ C$  and  $K_0$  is reversed value of thermal coefficient of resistivity at  $0^\circ C$ . The grid potential rise is:

$$GPR = I_g \cdot R_g \quad (7)$$

where  $I_g$  is maximum grid current in A and GPR is the ground potential rise in Volt. Allowable touch and step voltages are given in [25]; while the step voltage ( $E_s$ ) is obtained from [26]:

$$E_s = \frac{\rho \cdot K_s \cdot K_i \cdot I_G}{0.75L_{\square} + 0.85L_R} \quad (8)$$

$$I_G = D_f \times I_g \quad (9)$$

$$K_s = \frac{1}{\pi} \left[ \frac{1}{2h} + \frac{1}{D+h} + \frac{1}{D} \left( \square - 0.5^{n-2} \right) \right]$$

(10)

$$K_i = 0.644 + \square \cdot 148n \quad (11)$$

Where;  $E_s$  is Step voltage in V,  $I_G$  is maximum grid current that flows between ground grid and surrounding earth in A,  $D_f$  is decrement factor for determining  $I_G$ ,  $I_g$  is maximum grid current,  $K_s$  is spacing factor for step voltage,  $K_i$  is correction factor for grid geometry,  $h$  is depth of the grid in m. The mesh (touch) voltage ( $E_m$ ) is given by:

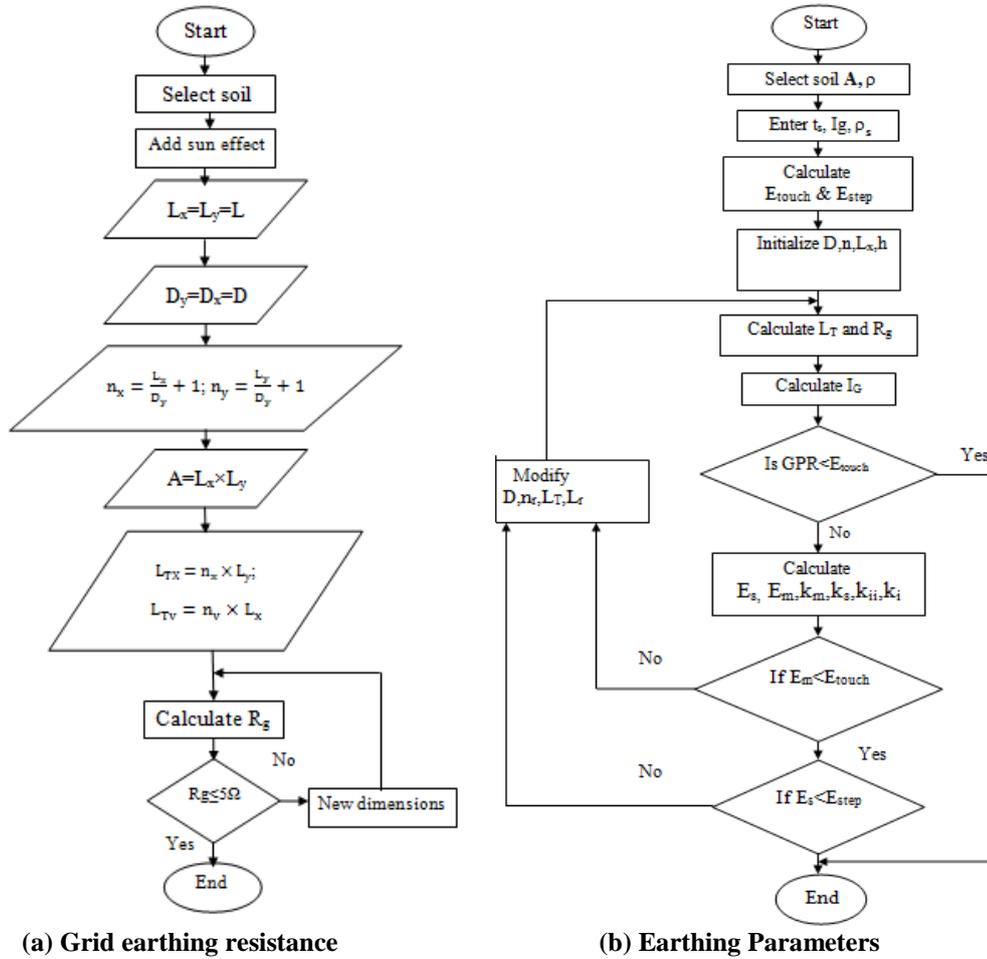
$$E_m = \frac{\rho \cdot I_g \cdot K_i \cdot K_m}{L_c + \left[ 1.55 + 1.22 \left( \frac{L_r}{\sqrt{L_x^2 + L_y^2}} \right) \right] \times L_R} \quad (12)$$

$$K_m = \frac{1}{2\pi} \left[ \ln \left( \frac{D^2}{16hd_r} + \frac{(D+2h)^2}{8Dd_r} - \frac{h}{4d_r} \right) \right] + \frac{K_{\square}}{k_h} \ln \left( \frac{8}{\pi(2n-1)} \right) \quad (13)$$

For grids with ground rods along the perimeter,  $K_{ii} = 1$ , or for grids with ground rods in the grid corners, as well as both along the perimeter and throughout the grid area. For grids with no ground rods or grids with only a few ground rods, none located in the corners or on the perimeter.

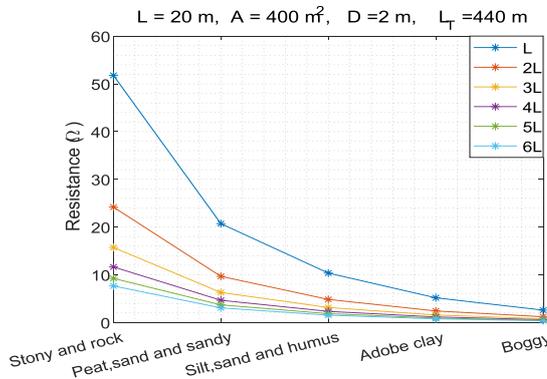
$$K_{ii} = \frac{1}{(2 \cdot n)^{\frac{2}{n}}}, \quad K_h = \sqrt{1 + \frac{h}{\square \cdot 0}} \quad \text{and} \quad h_0 = 1.$$

where;  $K_{ii}$  is Corrective weighting factor that adjusts for the effects of inner conductors on the corner mesh, and  $h_0$  is the grid reference depth. This work develops a simple and easy to use grounding parameters calculators according to the procedures of Fig.3.



**Fig.3: Earthing system calculators**

Most of the previously mathematical formulas are calculated according to the IEEE std-80 [26]. However, the grid cost is higher cost than the two other earthing techniques, it has the advantage of suitability for different soil types. The calculator of the grid earthing resistance will provide full earthing resistance description in a fast way for the earthing designer engineers. The flowchart of the grid resistance and ground system parameters calculators are shown in Fig.3 (a) and (b) respectively. In the grid calculator the square grid length ( $L_x=L_y=L$ ) and the spacing between the parallel conductors ( $D_x=D_y=D$ ) are the only data entry for obtaining the whole earthing resistance behavior for different soil types as depicted in figure 4.



**Fig.4: Grid calculator results**

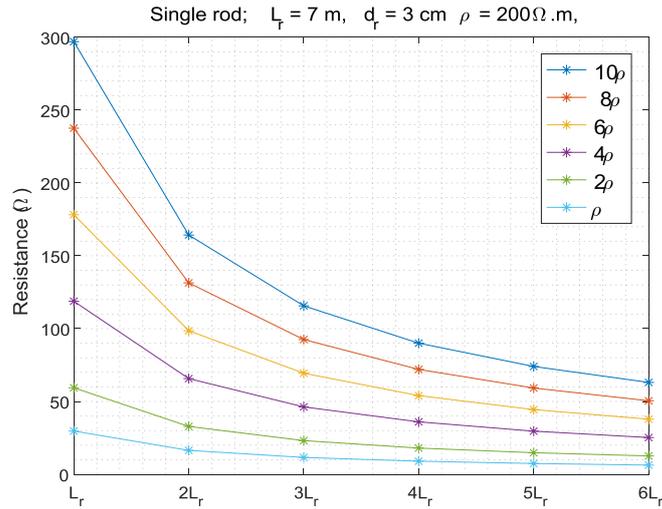
This calculator, in addition to study  $R_g$  in terms of either grid length, conductors spacing, soil types is allowing the user to consider the soil moisture state as well as monitoring the earthing resistance suitability in contrast with both mesh and step voltages.

**Results and analysis**

The results of this work can be classified into three different categories based the earthing effective parameters such as earthing electrodes type and dimension, soil type and the ambient temperature that directly effect on the soil moisture state.

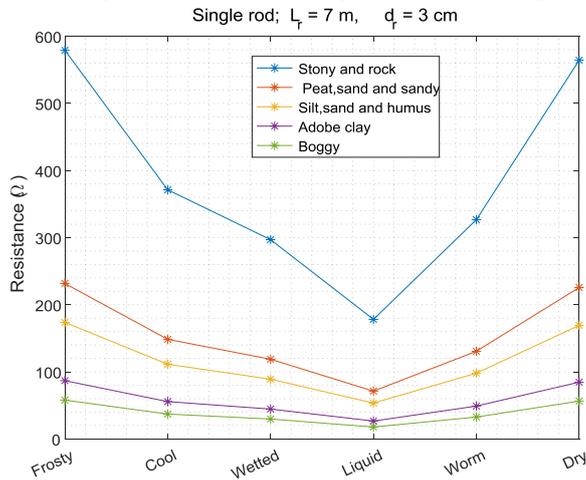
**Single rod**

A rod length of  $L=7\text{m}$  and diameter of  $3\text{cm}$  is resulting in about  $63\Omega$  earthing resistance for  $200\Omega\cdot\text{m}$  soil resistivity as shown in figure 5. This resistance ( $63\Omega$ ) can be decreased to about  $12.6\Omega$  for five times increasing the rod length ( $5L=35\text{m}$ ). On the other hand, the  $2000\Omega\cdot\text{m}$  soil resistivity with this rod dimensions results in an earthing resistance of  $297\Omega$  which may be reduced to about  $59.4\Omega$  by using a rod length of  $35\text{m}$ .



**Fig.5: Single rod arthing resistance (disabled moisture effect)**

Considering the moisture and the ambient temperature, the results have been dramatically changed. Figure 6 shows the significant increasing of the earthing resistance at both dry and



**Fig.6: Single rod with different soil moisture conditions**

frosty soils. For example, in case of  $200\Omega$  soil resistivity, the same  $7\text{m}$  rod length and  $3\text{cm}$  diameter bounds the earthing resistance around  $57\Omega$  for frosty and dry soil while  $17\Omega$  for the liquid moisture in the boggy soil. The variance of the earthing resistance is demonstrated according to the different soil types where  $R_g$  varies from  $17\Omega$  (boggy) to about  $570\Omega$  (stony and rock) as shown in Fig.6.

**Multi-rod**

The multiple rods for the grounding systems are considered especially in case of higher soil resistivity types. This scheme can be found in different arrangement such as parallel elec-

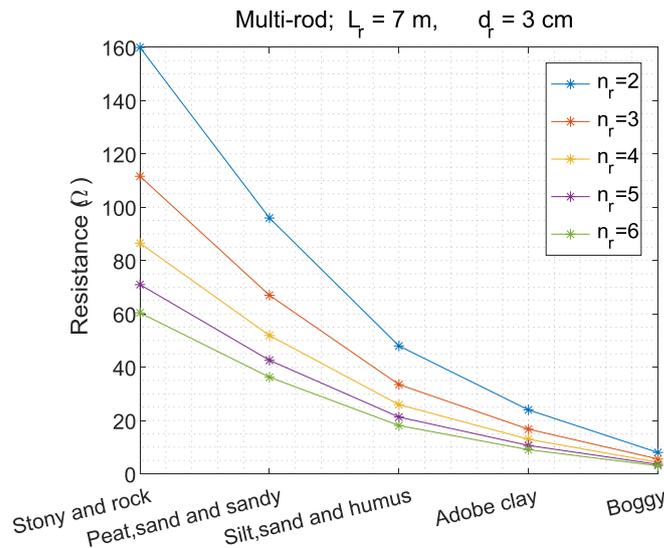
trodes in a line, a hollow square, equilateral triangle, or an L section. The form of the rods arrangement had no significant impact on the earthing resistance. Some of the multi-rod results in table.1 has been validated the mathematical approximation in equation (14).

**Table (1): Multi-rod calculated earthing resistances**

Case	No of rods(n)	$R_n$
1	2	10
2	3	6.6
3	4	5
4	5	4
5	6	3.3

$$R_n \approx \frac{R_g}{n} \quad (14)$$

Where:  $R_n$  is the total equivalent earthing resistance of the multi-rod system,  $R_g$  is the resistance of the single rod and  $n$  is number of rods. The earthing resistances of different soil resistivity with a multi-rod system are displayed in Fig.7.



**Fig.7: Parallel electrodes in line (disabled moisture effect)**

However, this topology is widely used, the higher cost and efforts are the challenges of recommending this topology. Considering the moisture states, for a soil resistivity  $2000\Omega.m$  (stony and rocky) and number of rods  $n_r=2$  the calculated earthing resistance are varied from  $289\Omega$  (frosty and dry) to around  $89\Omega$  (liquid moisture) as shown in Fig.8. this figure also shows improvement of the earthing resistance due increasing rod numbers to 6 rods, where the earthing resistance was  $96\Omega$  (frosty and dry) and about  $29\Omega$  (liquid moisture).

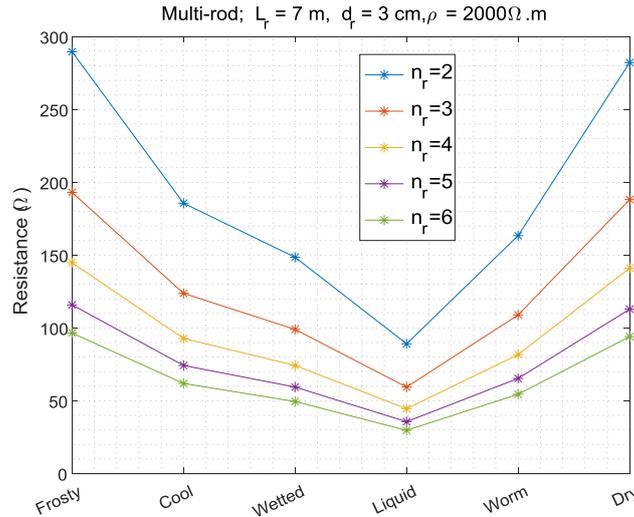


Fig.8: Parallel electrodes multi-rods with soil moisture

**Grid (lattice)**

The grid scheme is the commonly used for a higher resistance reduction through soil resistivity wide range. A grid of 20m length, 3m distance and changing the length from L (20m) to 6 L (120m) the stony and rocky grounding resistance lessening from 53.7Ω about to 2.1Ω respectively as shown in Fig.9.

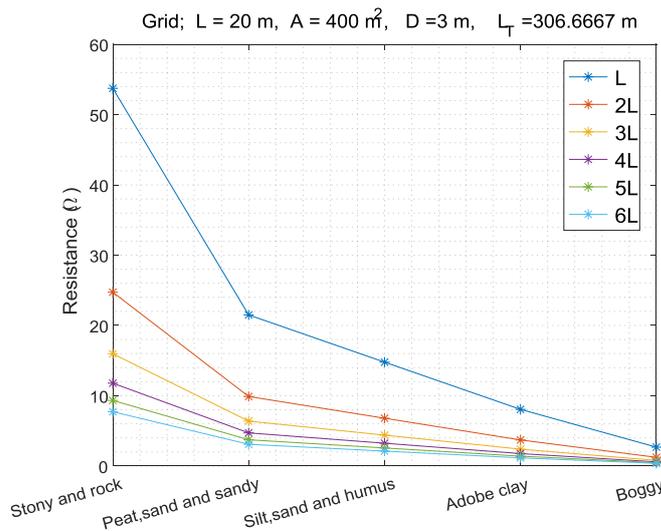


Fig.9: Effect of the grid length (disabled the moisture effect)

Similarly, 24.3Ω grounding resistance of peat, sand and sandy soil has been dropped to 1.06Ω. The decreasing of adobe clay earthing resistance from 9.3Ω to 0.4Ω is due to the same length increasing while the boggy earthing resistance decreased from 7.58Ω to 0.38Ω. the moisture effect is depicted in figure 10. The earthing resistance profile shows the reduction of  $R_g$  especially at the wetted moisture soil 42 Ω for stony and rocky soil.

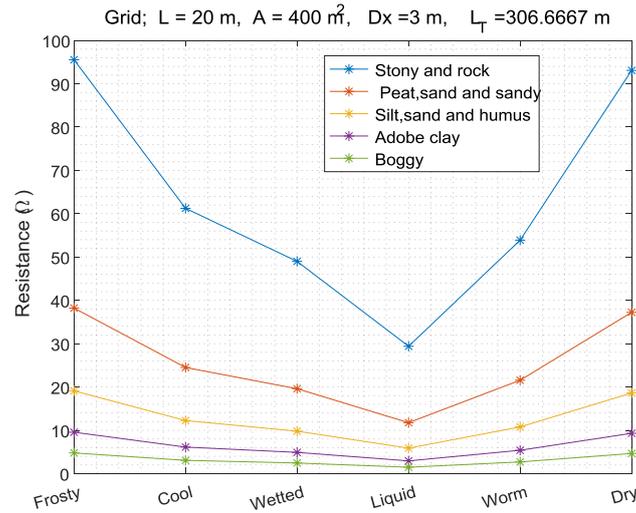


Fig.10: Grid earthing system with moistured soil

Using 180 m grid length for instance can accomplish the permissible values of  $R_g$  for all different soil types at all moisture states except stony and rocky soil as obvious in the figure 11.

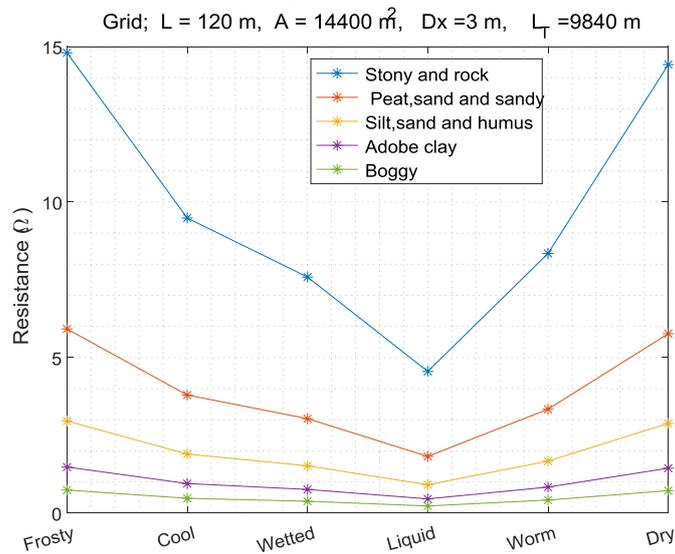


Fig.11:  $R_g$  of the 180 m grid length

One can add either the salts as improvement tools for these excepted soils or water tube. finally, the earthing resistances of the grid built-in rods 0, 5, 10 and 20 were 2.86, 2.89, 2.90, 2.92Ω respectively as listed in table 2. It is clear that the limited changes of the resistance and the step voltage while a significant touch voltage has been reached for zero built-in grid rods.

Table 2: Rods effect on the grid earthing parameters

No	Built-in rods	Touch voltage (V)	Touch allowable	Step Voltage(V)	Step Allowable(V)	GPR (V)	$R_g(\Omega)$
1	0	1465	737	680	2454	5867	2.92
2	5	1208	737	643	2454	5827	2.90
3	10	1120	737	610	2454	5791	2.9
4	20	977	737	553	2454	5728	2.86

## CONCLUSIONS

Significant extension due to the status of the soil moisture for realistic resistivity calculation has been discussed. Although, the importance of the earthing resistance reduction, this work highlighted the necessity of satisfying the allowable step and touch voltages. Earthing resistance in terms of the soil types, electrode dimension, and the sun states has been determined. The behavior of the frosty soil resistivity has been described. The results analysis had been showed that single rod is the most suitable earthing element in case of lower soil resistivity such as boggy soil while multi rod for other types of soil which has characteristic of high resistivity should be used on the other side there are some types of soil look like stony and rocky soil grid must be used as earthing element that's due to its huge resistivity. The grid earthing scheme offered further reduction of the earthing resistance that is almost linearly proportional to total grid length. The results show that both the grid shape and the rod diameters have limited effect on the earthing resistance reduction.

## fo tsil Abbreviations

I	Current
V	Potential
$\pi$	$\pi \approx 3.14$
$\rho$	Resistivity of soil in $\Omega.m$
A	Equally spaced between two adjacent probes(m)
B	Un equally spaced of test probes(m)
$\Omega$	Ohm
P	Apparent resistivity of different layers( $\Omega.m$ )
$^{\circ}C$	Celsius
$R_g$	Resistance of the soil in $\Omega$
$L_r$	Length of the single rod in m
$d_r$	Diameter of the single rod in m
$\lambda$	Factor of rod numbers
$R_{n_e}$	Resistance of soil due to using multi-rod
S	Rod spacing in m
$R_1$	Resistance of one footing in $\Omega$
$L_C$	Total length of the conductor in the horizontal grid in m
$L_p$	Peripheral length of the grid in m
$L_x$	Maximum length of the grid in the x direction in m
$L_y$	Maximum length of the grid in the y direction in m
$D_m$	Maximum distance between any two points on the grid in m
N	Number of x-axis or y-axis
D	Spacing between conductors of grid in m
$L_R$	Total length of rods in the grid
$A_c$	Conductor size in sq-mm
$I_f$	Maximum fault current in kA
$t_c$	Duration of fault in sec
$\alpha_r$	Coefficient of resistivity at reference temperature
$\rho_r$	Resistivity of earth electrode at reference temperature $\mu\Omega/cm$
$T_m$	Maximum allowable temperature of conductor in $^{\circ}C$
$T_a$	Ambient temperature in $^{\circ}C$
Ko	Reversed value of thermal coefficient of resistivity at $0^{\circ}C$
$I_g$	Maximum grid current in A
$C_s$	Derating factor of surface layer resistivity and 1 for no protective surface layer
$\rho_s$	Resistivity of the surface material in $\Omega.m$
$t_f$	Fault duration time in sec
$E_{touch}$	Tolerable touch voltage for human
$E_{step}$	Tolerable step voltage for human
$E_s$	Step voltage between a point above the outer corner of the grid and a point 1 m diagonally outside the grid for the simplified method in V
$I_G$	Maximum grid current that flows between ground grid and surrounding earth in A
$D_f$	Factor of decrement for determining $I_G$

$K_s$	Factor of spacing for step voltage simplified method
$K_i$	Factor of correction for grid geometry
$H$	Depth of the grid in m
$E_m$	Mesh voltage in V
$K_{ii}$	Factor of the corrective weighting that adjusts for effects of inner conductors on mesh corner, simplified method
$H_o$	Grid reference depth
$a_1$	Hemisphere radius and round plate radius in m
$d_{ring}$	Diameter of ring in m
$d_{wire}$	Diameter of wire in m

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